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Kerr comb generation with suppressed cavityoptomechanical oscillation in toroid microcavity

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Kerr frequency comb



Kerr comb

Microcavity



- √ Small & Inexpensive
- ✓ High repetition rate (10GHz-1THz)
- ✓ Large bandwidth
- ✓ Low threshold pump

Threshold pump power for four-wave mixing

 $P_{\rm threshold} \propto V/Q^2$

V : Mode volumeQ : Quality factor

Conventional frequency comb sources

Ti:Sapphire laser



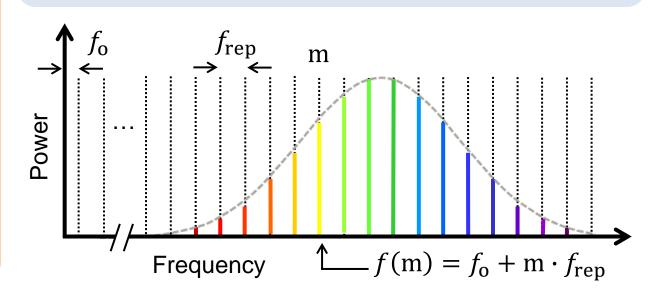
http://www.mpq.mpg.de/~haensch/comb/index.html

Fiber laser



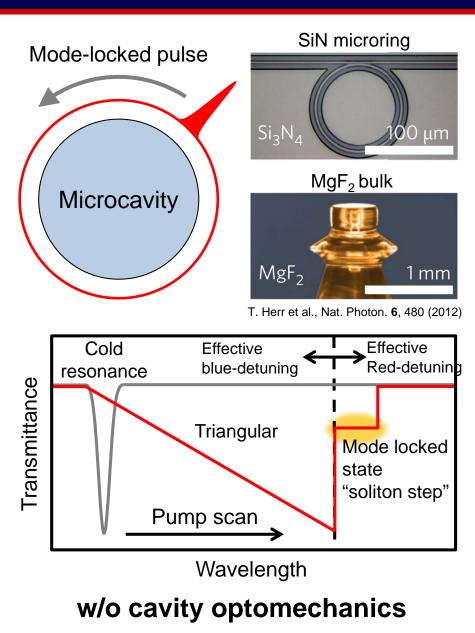
https://www.aist.go.jp/index_ja.html

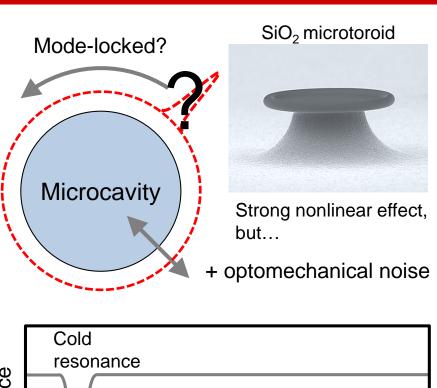
Large & Expensive

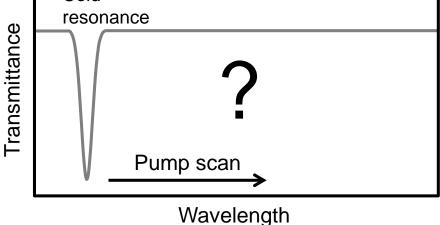


Motivation





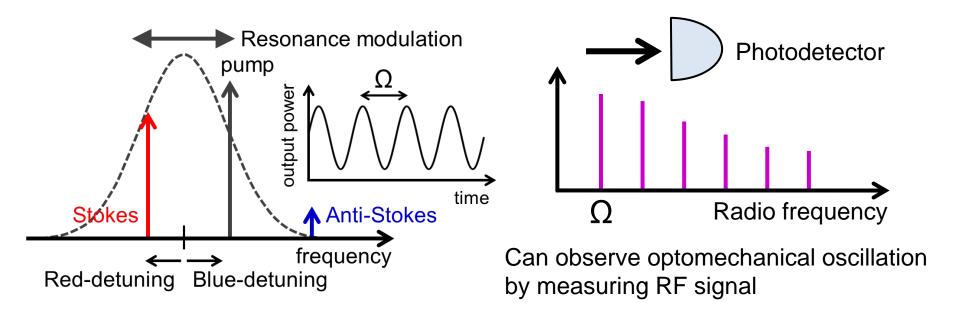


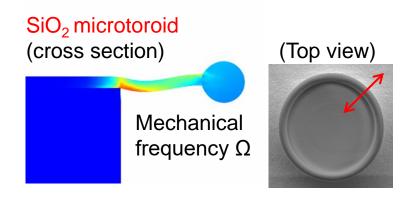


w/ cavity optomechanics

Cavity optomechanical oscillation



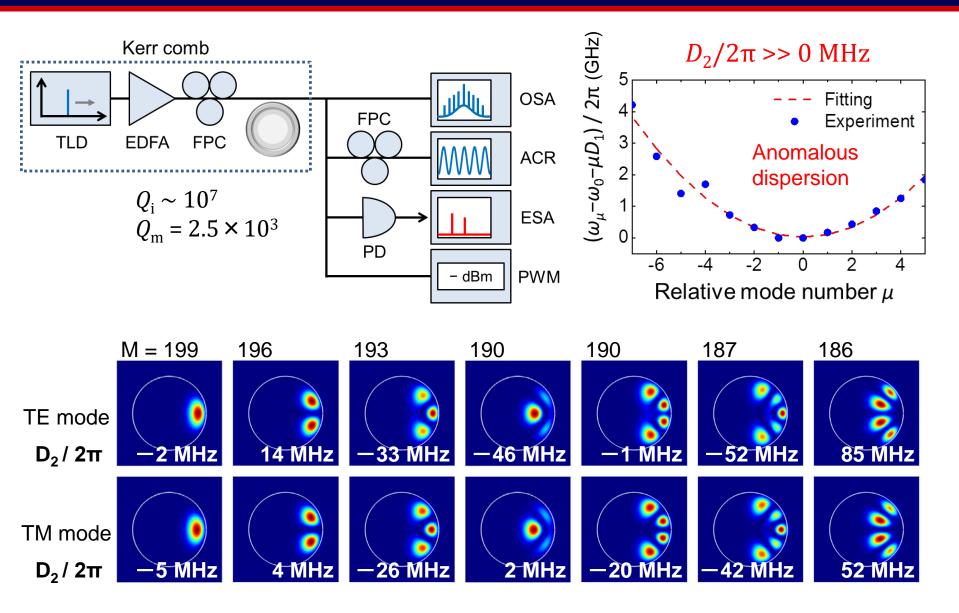




Blue-detuning Amplify optomechanical oscillation Red-detuning Suppress optomechanical oscillation

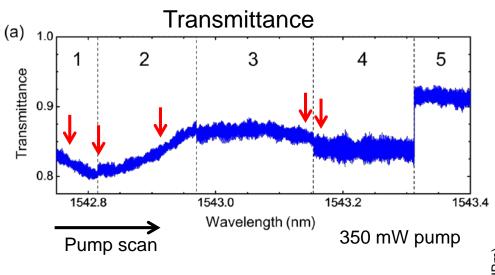
Experimental setup & Dispersion







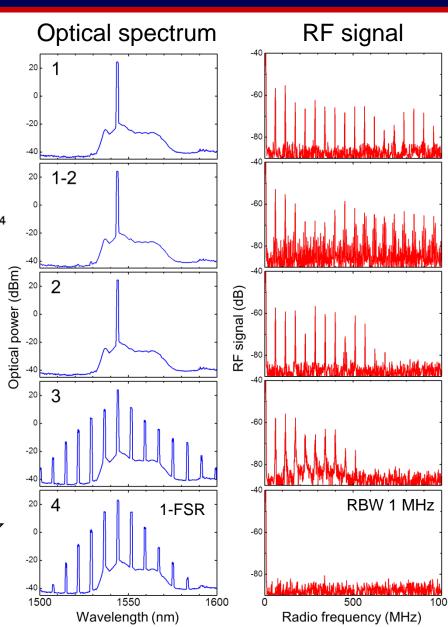




Multiple of 60 MHz signals were caused by optomechanical oscillation

RF signal disappeared

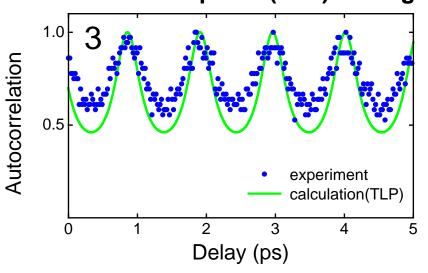
In terms of cavity optomechanics, state-4 is into effective red-detuning

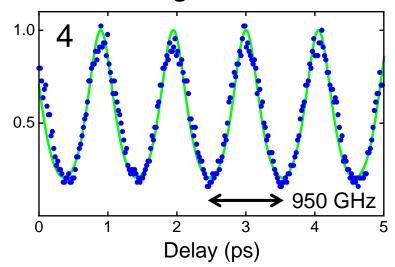


Autocorrelation waveform measurement

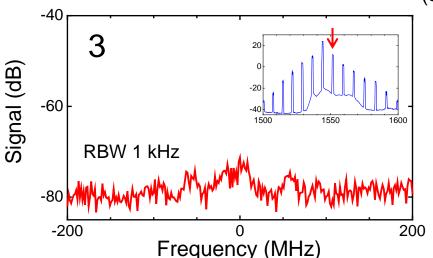


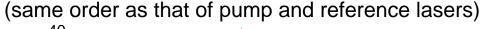
Transform limited pulse (TLP) of single-FSR comb was generated

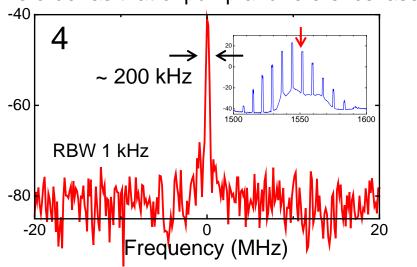




Linewidth of comb line

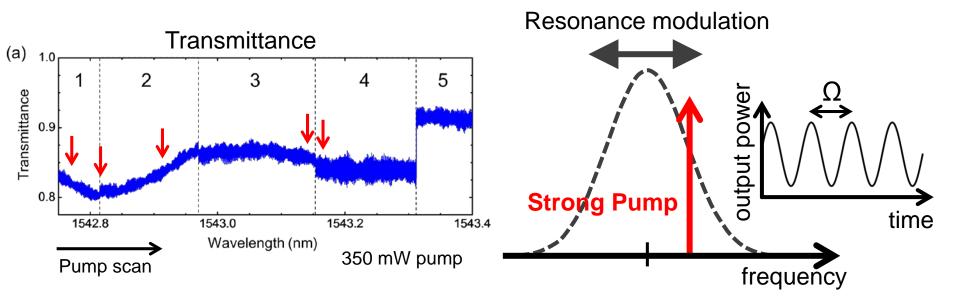






Transmittance affected by oscillation





Resonance modulation by optomechanical oscillation

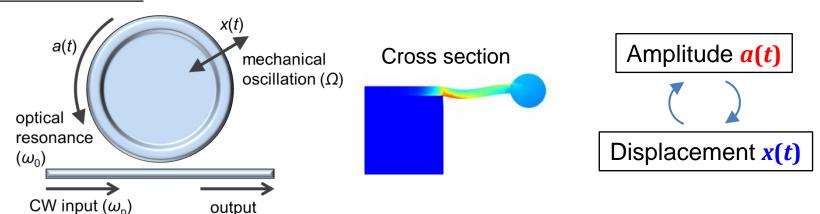
⇒ Chang transmittance?

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Simulation of transmittance



Simulation model



Previous research

T. Carmon et al., Phys. Rev. Lett. 94, 223902 (2005).

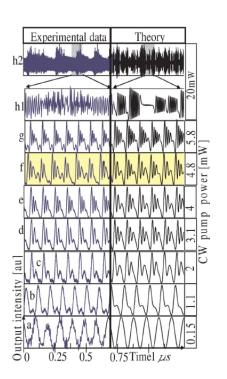
Slowly varying field amplitude in microcavity a(t):

$$\frac{d\boldsymbol{a}(\boldsymbol{t})}{dt} = -\boldsymbol{a}(\boldsymbol{t}) \left(\frac{\omega_0}{2Q_t} - i \left(\omega_p - \omega_0 + \boldsymbol{x}(\boldsymbol{t}) \frac{\omega_0}{R} \right) \right) + s_{in} \sqrt{\frac{\omega_0}{Q_c} FSR}$$
Optomechanical oscillation (resonance modulation)

Displacement in radial direction x(t):

$$\frac{d^2x(t)}{dt^2} + \frac{\Omega}{Q_{\rm m}} \cdot \frac{dx(t)}{dt} + \Omega^2x(t) = \frac{2\pi n}{m_{\rm eff}c} |a(t)|^2$$

 $ω_0$: resonance frequency, $ω_p$: pump frequency, Q_t : total Q, Q_c : coupling Q, s_{in} : input pump field, *FSR*: cavity FSR, *R*: cavity radius, *n*: refractive index,, c: speed of light, Ω: mechanical frequency, Q_m : mechanical Q, m_{eff} : effective mass



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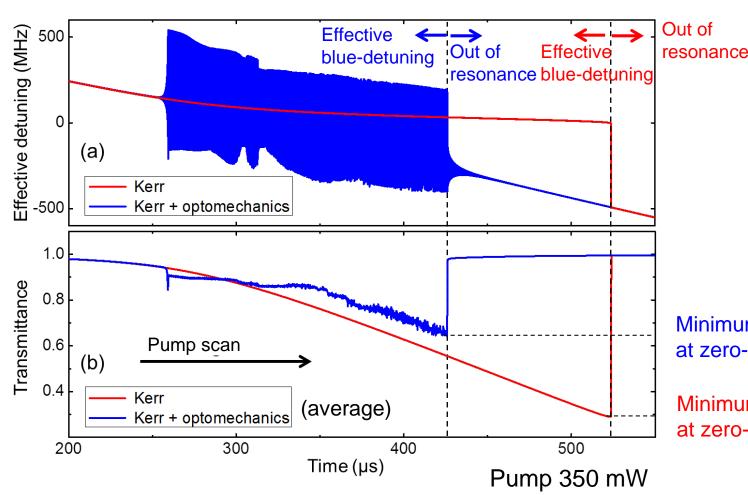
Effective detuning & Transmittance with high power pump



Slowly varying field amplitude in microcavity *a*(*t*):

$$\frac{da(t)}{dt} = -a(t) \left(\frac{\omega_0}{2Q_t} - i \left(\omega_p - \omega_0 + \Delta n_{\text{Kerr}}(t) \frac{\omega_0}{n} + x(t) \frac{\omega_0}{R} \right) \right) + s_{\text{in}}(t) \sqrt{\frac{\omega_0}{Q_c}} FSR$$
Kerr effect Optomechanical oscillation

Not including FWM process



Minimum transmittance at zero-detuning

Minimum transmittance at zero-detuning

Summary



- A mode-locked pulse with a single FSR was generated from a toroid microcavity although no "soliton step" was observed.
- A Kerr comb in a low noise state had a linewidth of 200 kHz, which is same order as that of a pump and a reference lasers.
- We calculated the influence of optomechanical oscillation on transmittance by considering Kerr and optomechanical effects.

Acknowledgements



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