

Asia Communications and Photonics Conference:
PR Workshop on Microcavity Photonics
Talk 6

Broad bandwidth phase-matched four-wave mixing in dispersion-engineered microresonators

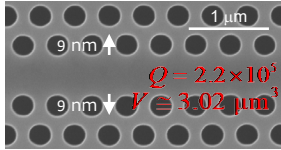
Takasumi Tanabe¹

Shun Fujii¹, Yuka Hayama², Koshiro Wada¹, and Yasuhiro Kakinuma²

1. Department of Electronics and Electrical Engineering,
Faculty of Science and Technology, Keio University
2. Department of System Design Engineering,
Faculty of Science and Technology, Keio University

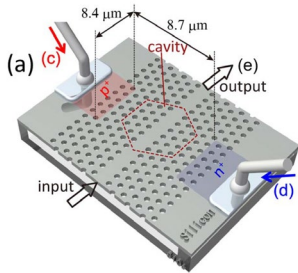


□ High-Q PhC nanoresonator



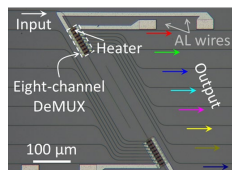
Y. Ooka, *et al.*, *Sci. Rep.* **5**, 11312 (2015).

□ Si PhC photo receiver/modulator

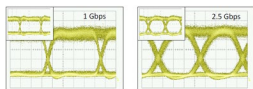


N. Daud, *et al.*, *AIP Adv.* **8**, 105224 (2018).
Y. Ooka, *et al.*, *Opt. Express*, **24**, 11199 (2016).

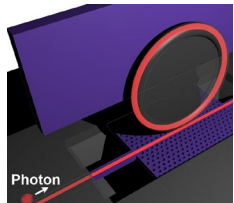
□ Si PhC WDM filter & other



Y. Ooka, *et al.* *Opt. Express* **25**, 1521 (2017).

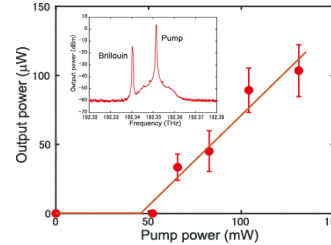


□ Coupling WGM w/ PhC



Y. Zhang, *et al.*, *Opt. Lett.* (2019) in press.

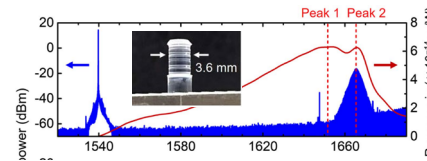
□ Brillouin laser & opto mechanics



R. Suzuki, *et al.* *Opt. Express* **25**, 28806 (2017)

Y. Honda, *et al.*, *Appl. Phys. Lett.* **112**, 201105 (2018).

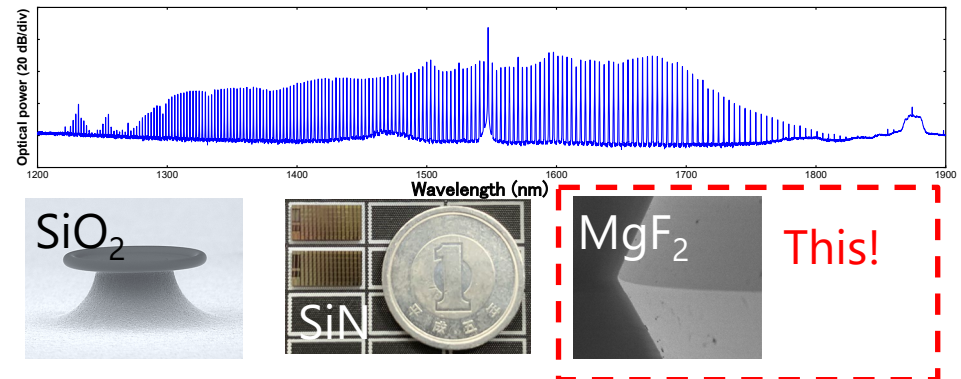
□ Raman comb & Er doped + CNT toroid



R. Suzuki, *et al.*, *J. Opt. Soc. Amer. B* **35**, 933 (2018).

T. Kumagai, *et al.* *J. Appl. Phys.* **123**, 233104 (2018).

□ FWM & microresonator frequency comb



S. Fujii, *et al.*, *J. Opt. Soc. Amer. B* **35**, 100 (2018).

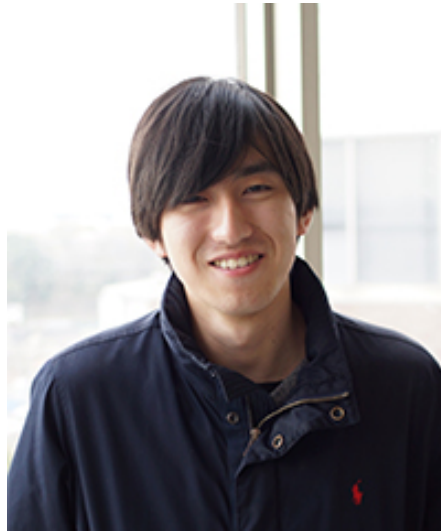
S. Fujii, *et al.*, *Opt. Lett.* **44**, 3146 (2019).



Design & measurement



Shun Fujii



Koshiro Wada

Ultra-precision fabrication



Yuka Hayama



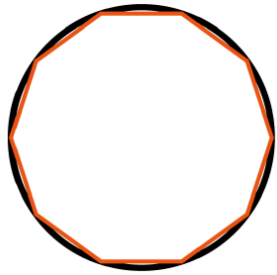
Prof. Yasuhiro Kakinuma



1. Background and motivation
2. Dispersion engineering of MgF₂ microresonators
3. Fabrication by computer-controlled turning
4. Phase-matched four-wave mixing (μ -comb generation)
5. Conclusion



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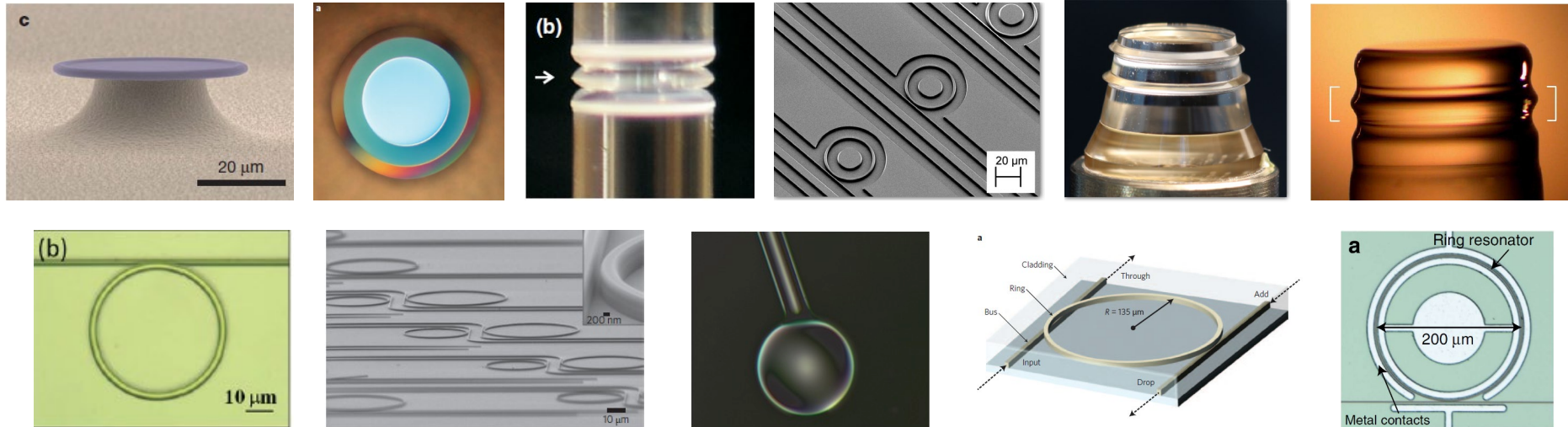


Whispering gallery mode (WGM) optical microresonator

Confines light for long photon lifetime (high Q) and has small volume

Enhances light-matter interaction in dielectric material

Dielectric microresonator platforms (Caltech, NIST, EPFL, OEwaves, Columbia, Harvard, Yale, INRS-EMT)



$$(\text{Intracavity power}) = \frac{4\eta d_1 Q}{\omega_0} \times (\text{Input power})$$

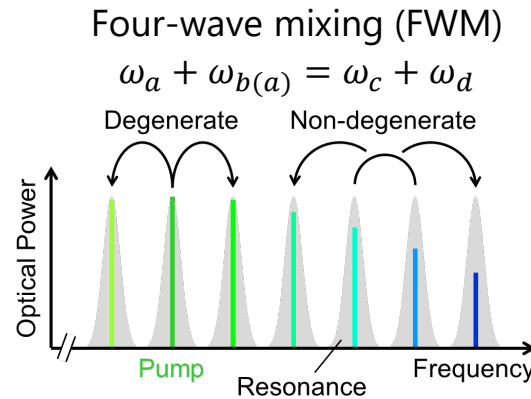
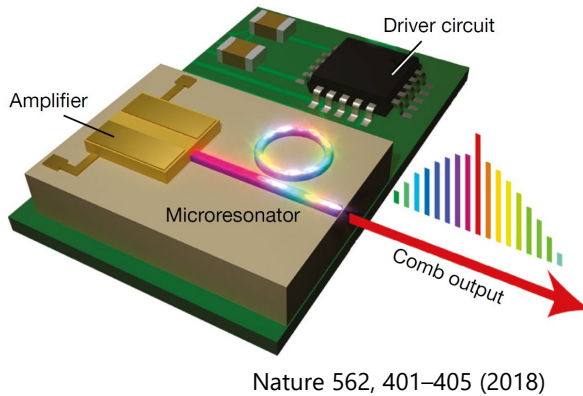
ω_0 : laser frequency, d_1 : cavity FSR,
 Q : quality factor, η : coupling parameter

e.g. $\omega_0/2\pi = 193$ THz, $d_1 = 100$ GHz,
 $Q = 1 \times 10^8$, $\eta = 0.5$ (critical coupling)

10 mW input \Rightarrow 165 W intracavity



Target application: Microresonator frequency comb (Kerr comb)

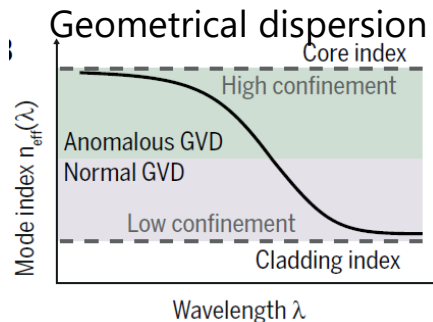
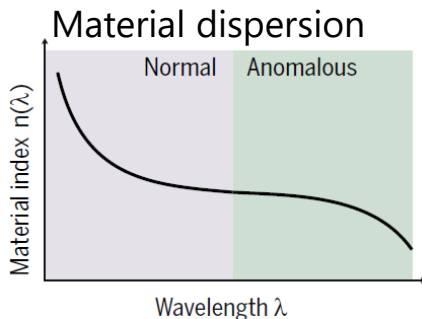


Threshold power for FWM

$$P_{\text{th}} = \frac{\kappa^2 n_0^2 V_{\text{eff}}}{8\eta \omega_0 c n_2} \propto \frac{V}{n_2 Q^2}$$

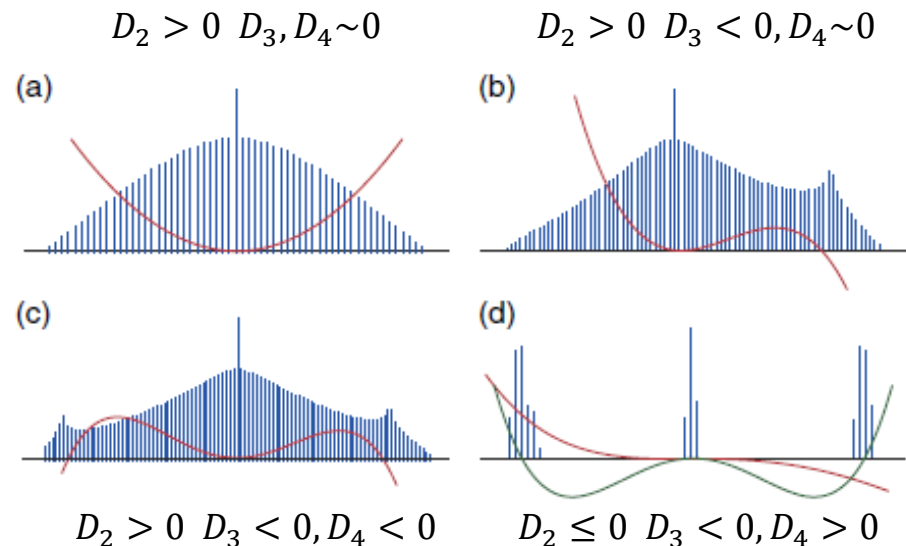
- Compact size
- Low energy consumption
- Broad bandwidth
- Large mode spacing ~ 1000 GHz

Microresonator dispersion and the effect on microcomb spectrum



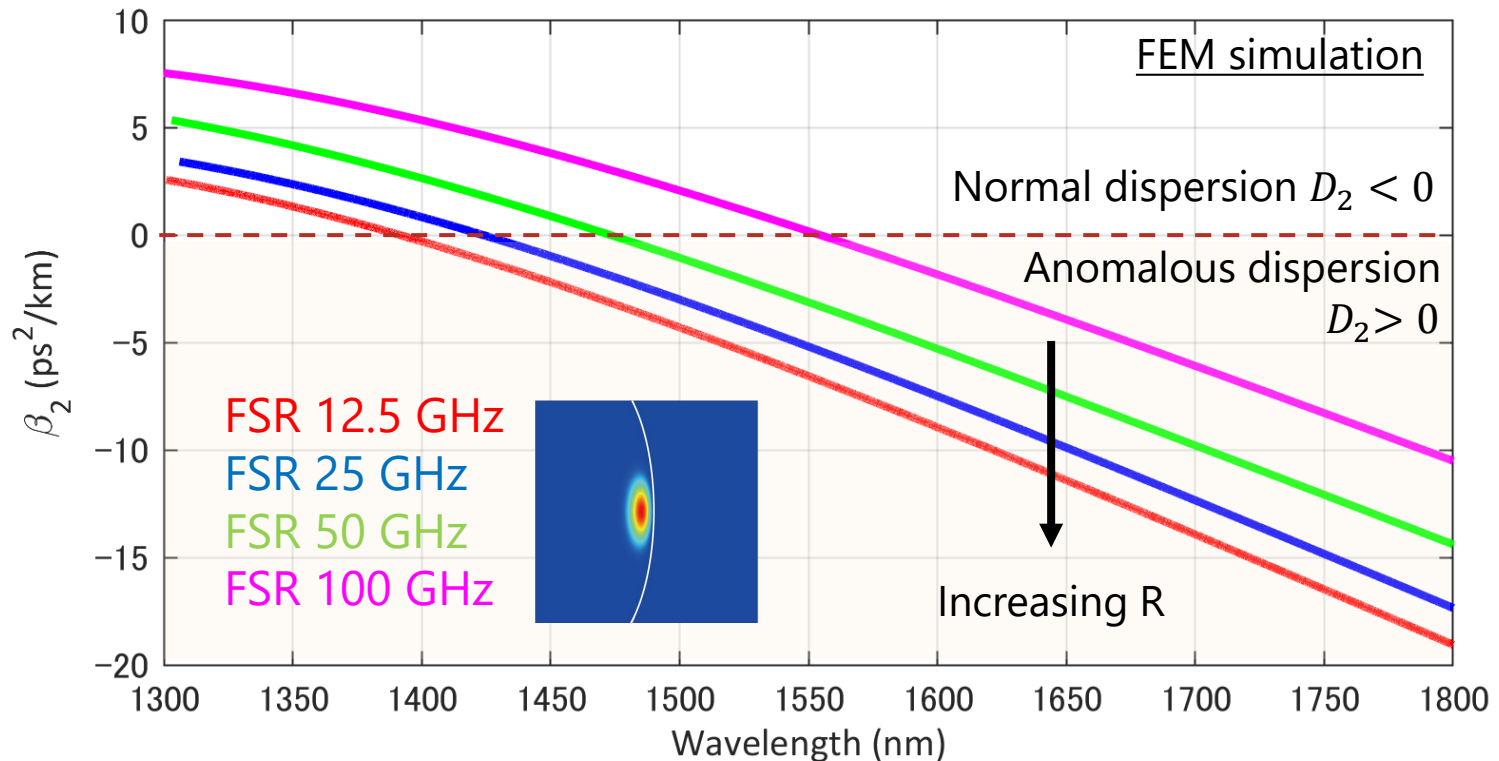
Sign and value of D_n determines optical spectrum

$$\omega_\mu = \omega_0 + D_1\mu + \frac{1}{2}D_2\mu^2 + \frac{1}{6}D_3\mu^3 + \frac{1}{24}D_4\mu^4 \dots$$





GVD parameters β_2 for MgF₂ microresonators with different FSRs



- 100 GHz FSR microresonator shows weak normal dispersion in 1550 nm band
- Geometrical dispersion limits microcomb generation in small-R MgF₂ resonator



Fabrication method of crystalline microresonator

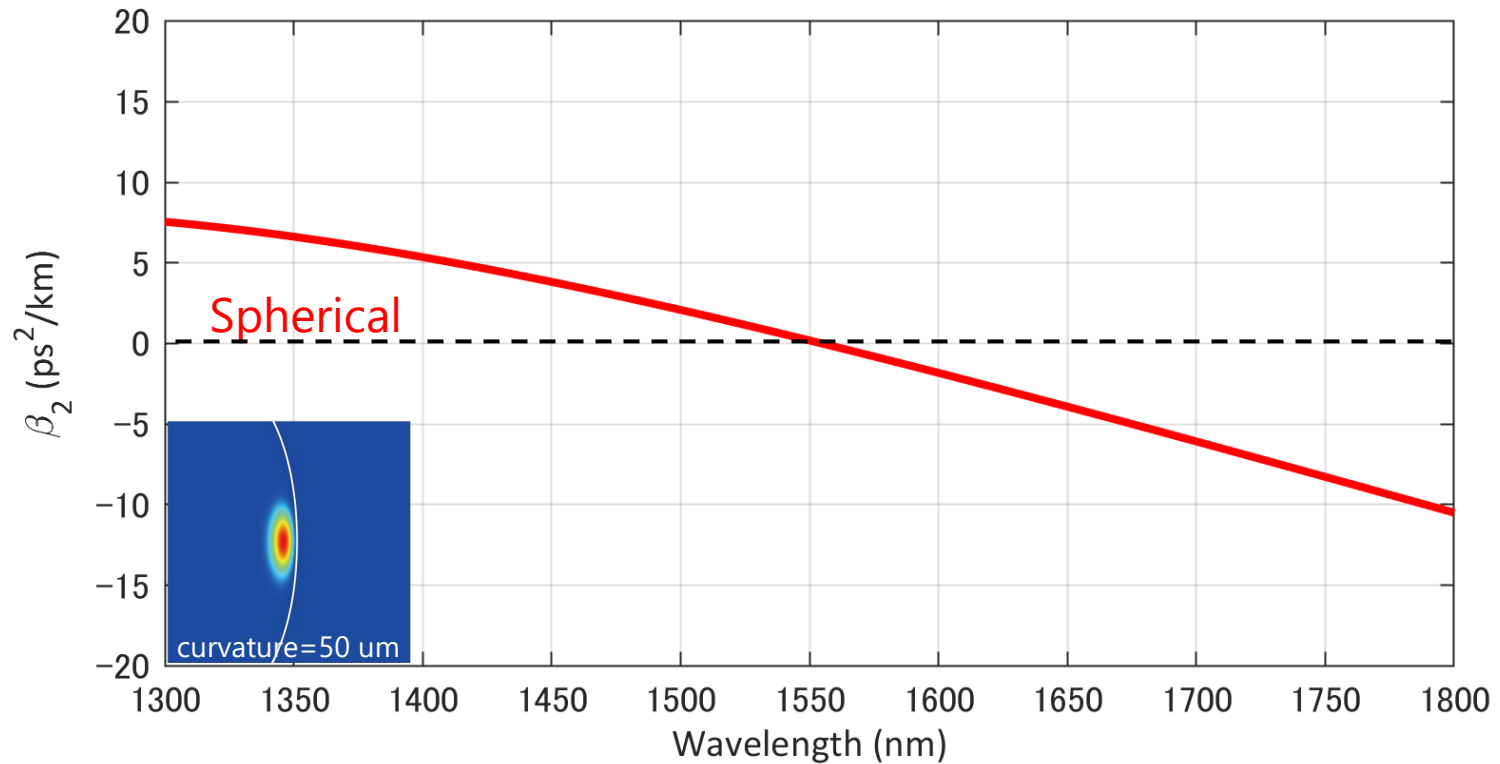
Hand Polishing	Fluoride crystal	$Q \sim 10^{10}$	Ultra-high Q Form accuracy ✘
	MgF ₂ CaF ₂ BaF ₂		
Machining	LiNbO ₃ (PPLN)	$Q \sim 10^8$	High-Q Form accuracy ○

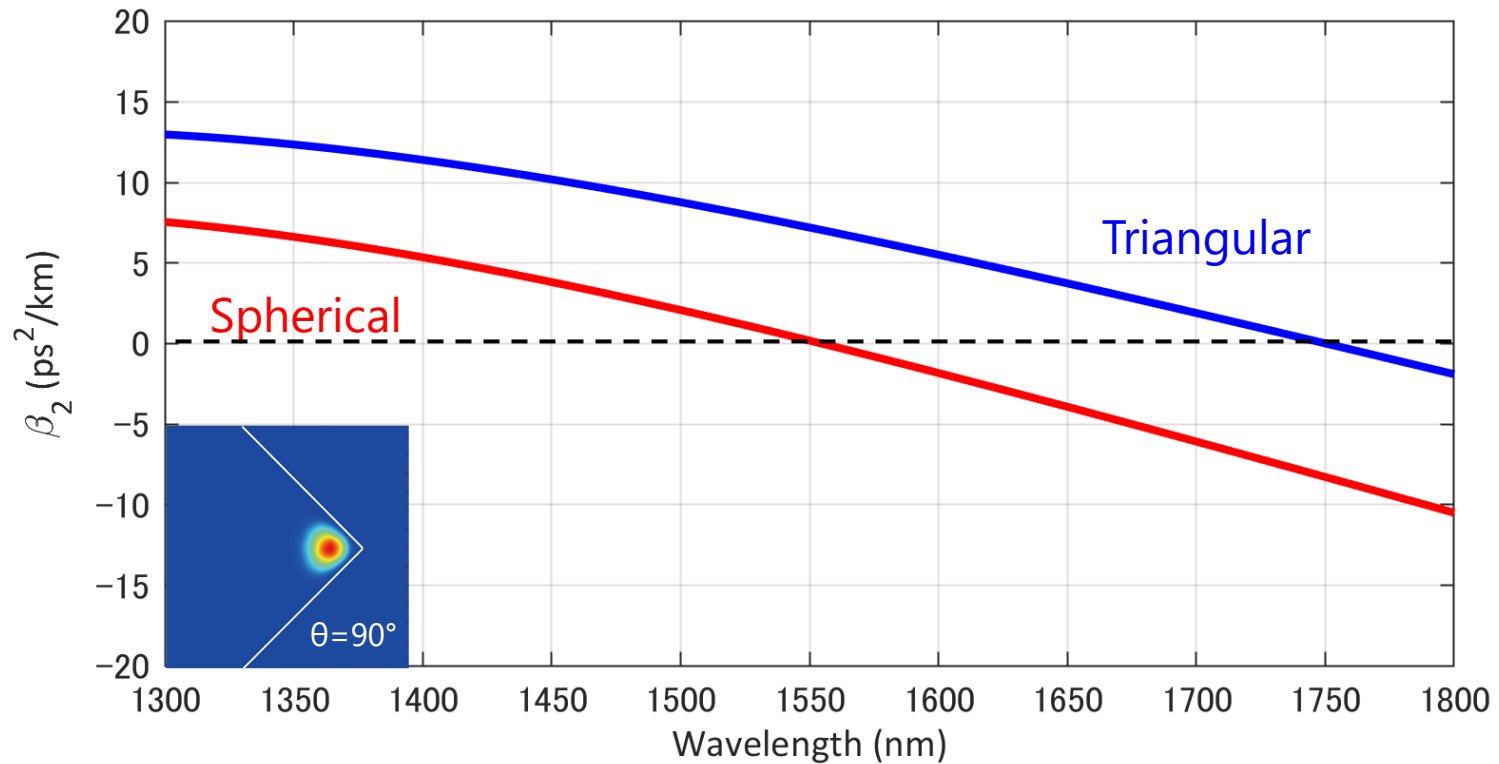
- Fabricate ultra-high Q crystalline microresonators ($Q > 10^8$) by computer-controlled machining **without polishing process**
- Explore resonator cross-section which realizes anomalous dispersion for 100 GHz free-spectral range (FSR) crystalline microresonators

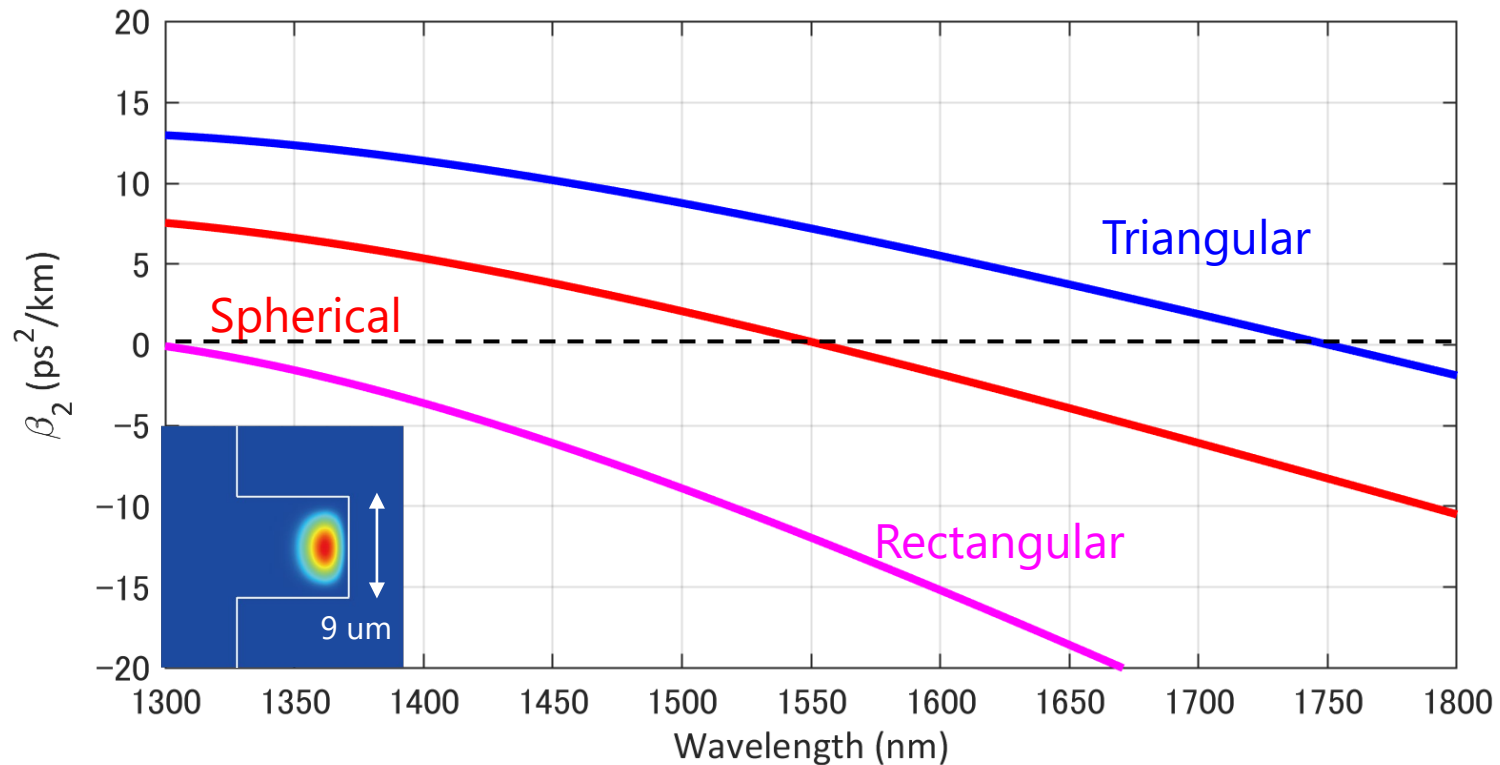
Overcome Q limitation to achieve 100 GHz FSR microcomb generation

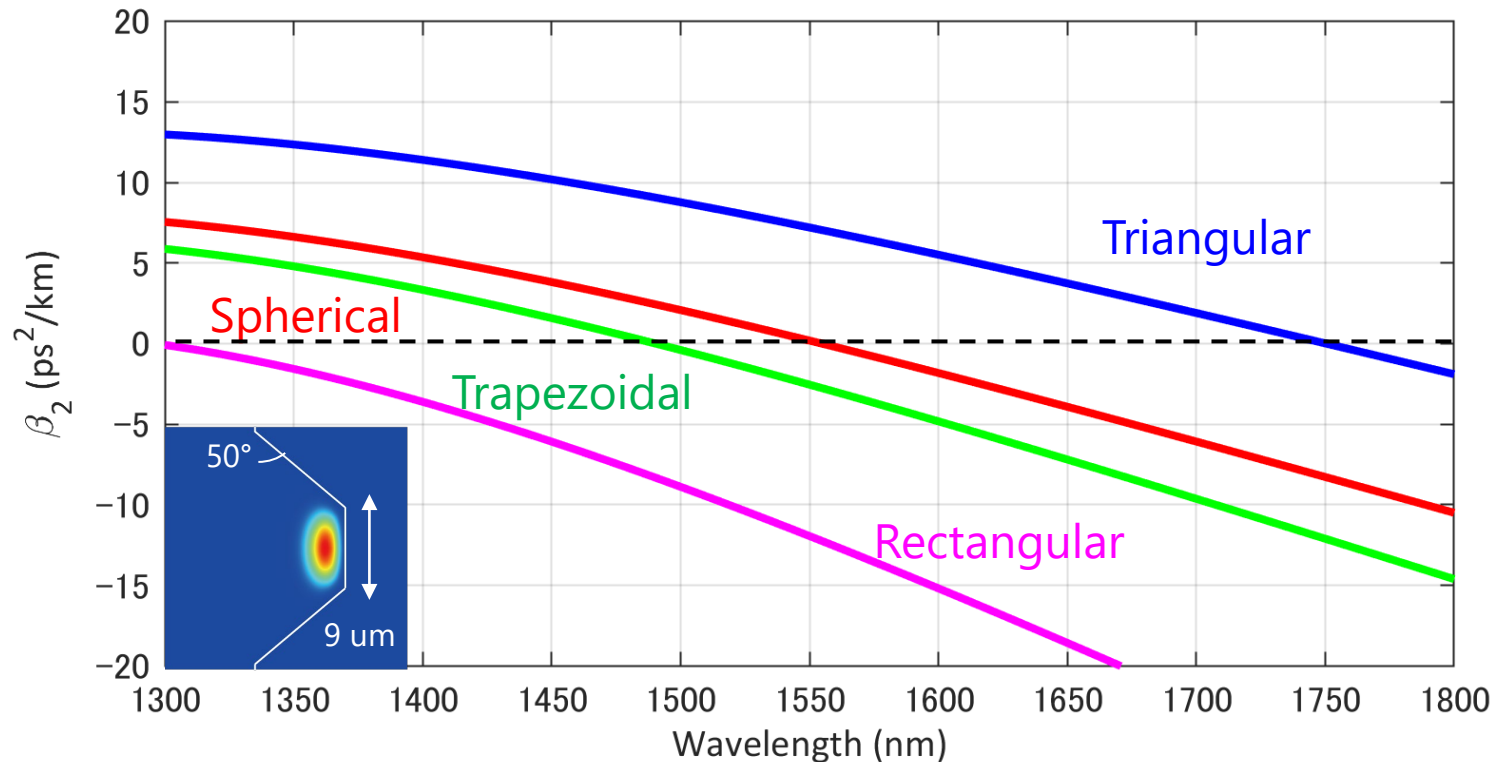


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GVD parameters β_2 for "100 GHz" MgF₂ microresonators

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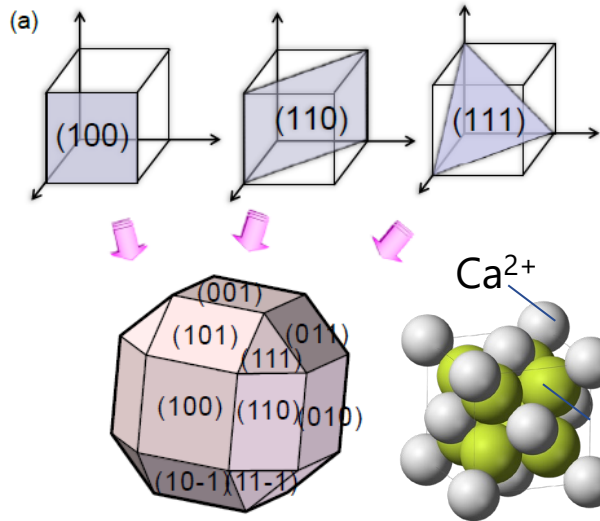
- Degree of freedom of structures allows us to control resonator dispersion
- Rectangular shape is ideal for realizing anomalous group-velocity dispersion



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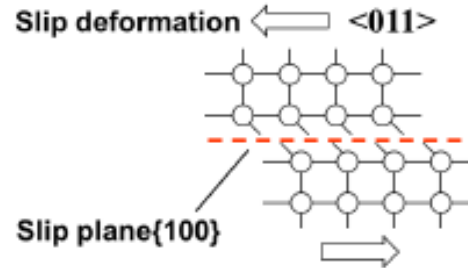


Crystallographic image of CaF₂ material

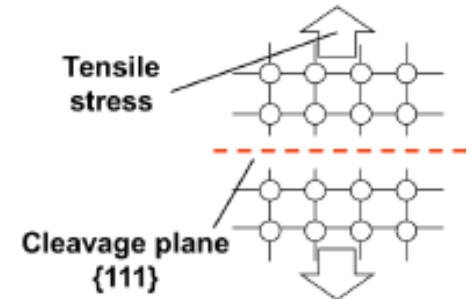


- Plane of single crystal is defined as mirror index
- CaF₂ consists of only 3 planes (100), (110), (111)
- Cutting mode transition observed with cutting depth

Slip formation (100)[110]

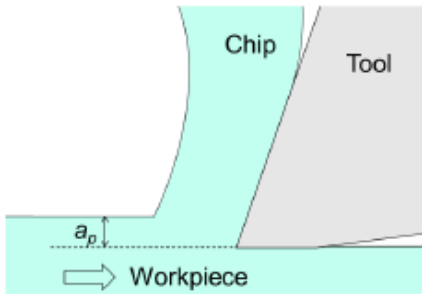


Cleavage formation (111)

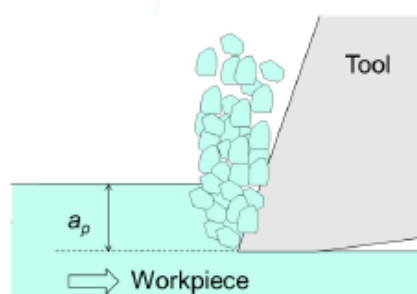


Cutting mode transition is observed depending on crystal anisotropy

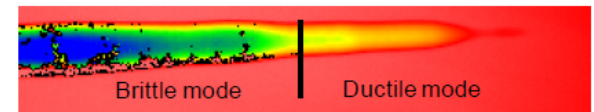
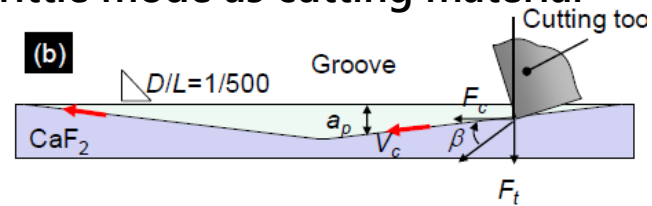
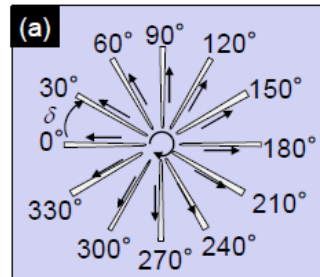
Ductile-mode cutting



Brittle-mode cutting



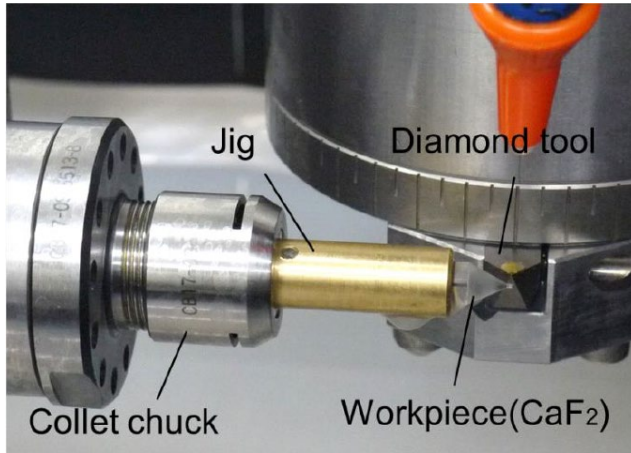
Transition to brittle mode as cutting material



Cutting depth < Critical depth Cutting depth > Critical depth

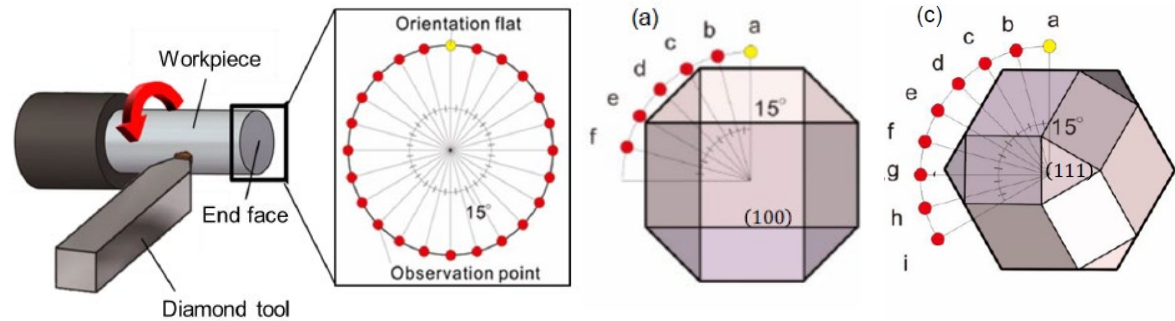


Experimental setup

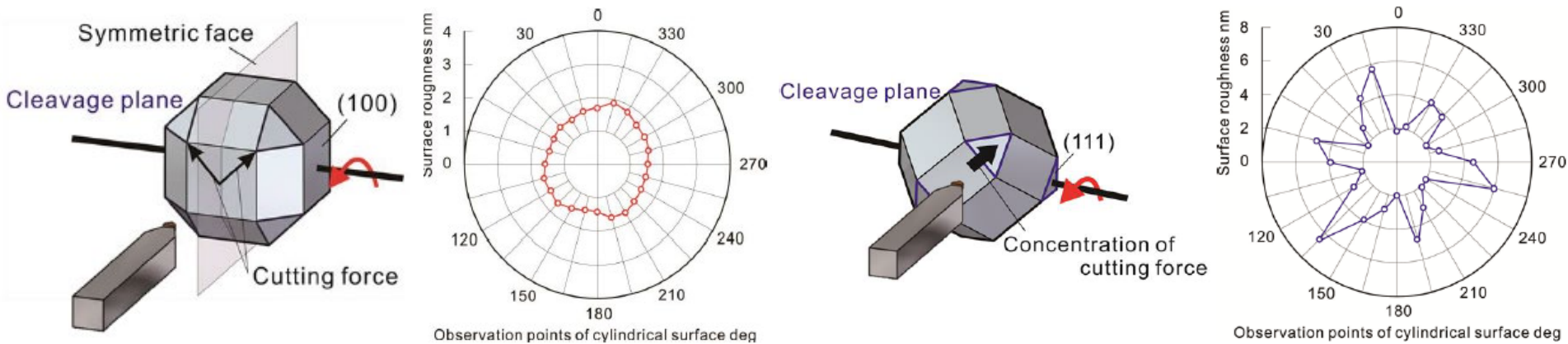


“Objective” of cylindrical turning experiment

- Cutting plane and direction are continuously and simultaneously changed when resonator is turned
- Investigate surface roughness of entire cylindrical surface



Cylindrical surface roughness for observation points with different end-faces

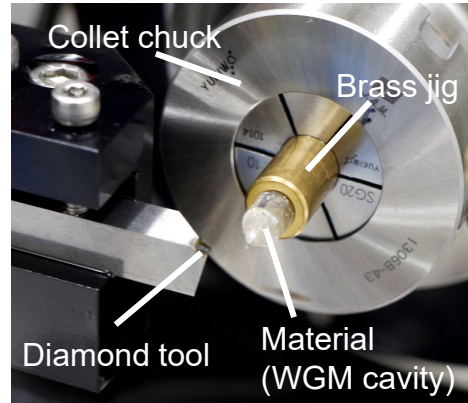


Observed smooth surface with end-face (100)

Observed surface clack with the end-face (111)



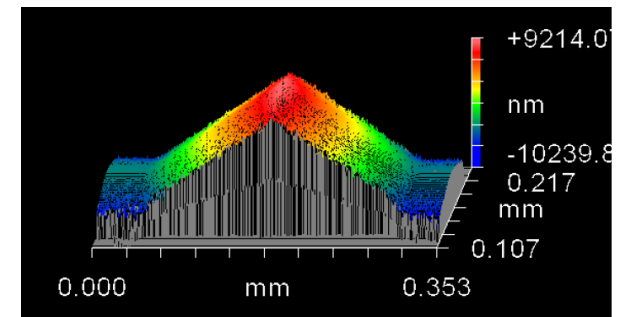
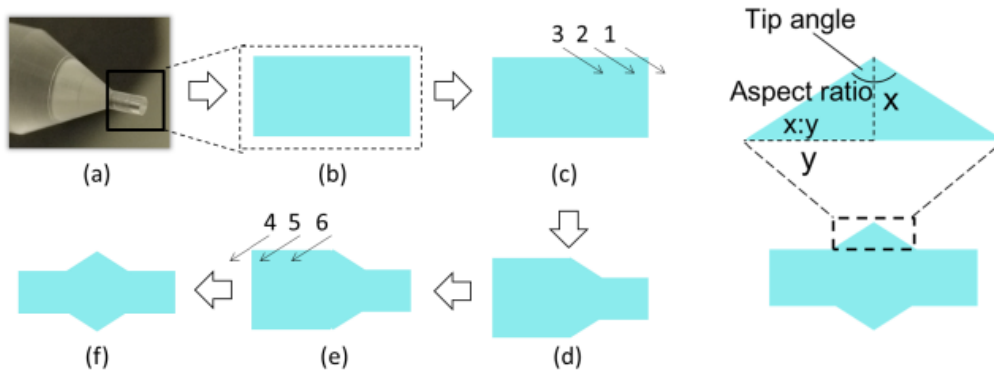
Experimental setup and machine used



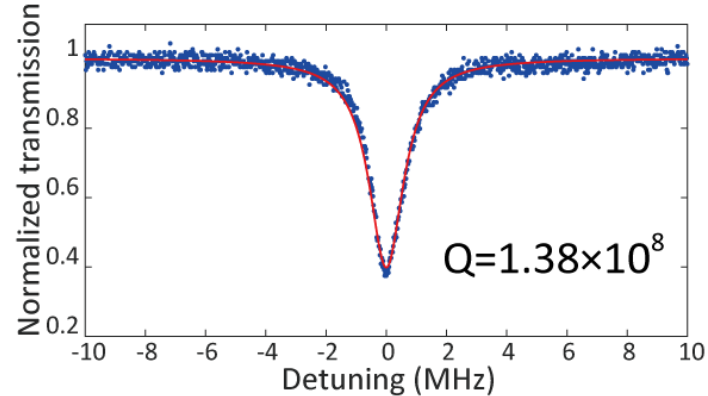
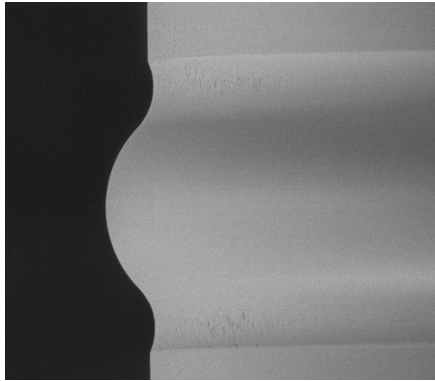
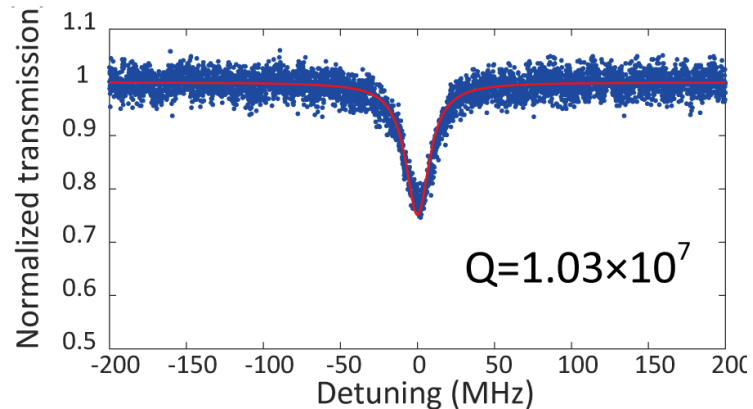
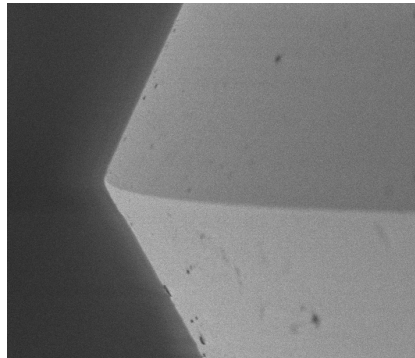
Manufacturing parameters

- Rotation speed [min^{-1}]
- Cutting speed [m/min]
- Feed per revolution [$\mu\text{m}/\text{rev}$]
- Depth of cut [nm]
- End-face orientation
- Lubricant
- Nose radius (cutting tool)
- Rake angle (cutting tool)

Fabrication flow of ultra-precision turning for *triangular* cross-section microresonator



- The tip angle and the aspect ratio are pre-designed and formed by computer-controlled turning, which is attractive with respect to dispersion engineering

Crystalline microresonator fabricated "*without polishing*"Spherical MgF_2 WGM Diameter 508 μm Curvature 36 μm Triangular CaF_2 WGM Diameter 502 μm Apex angle 120°

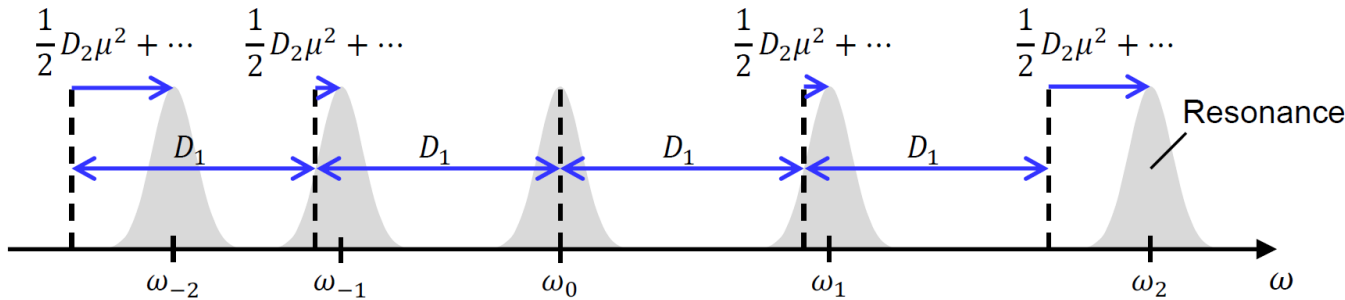
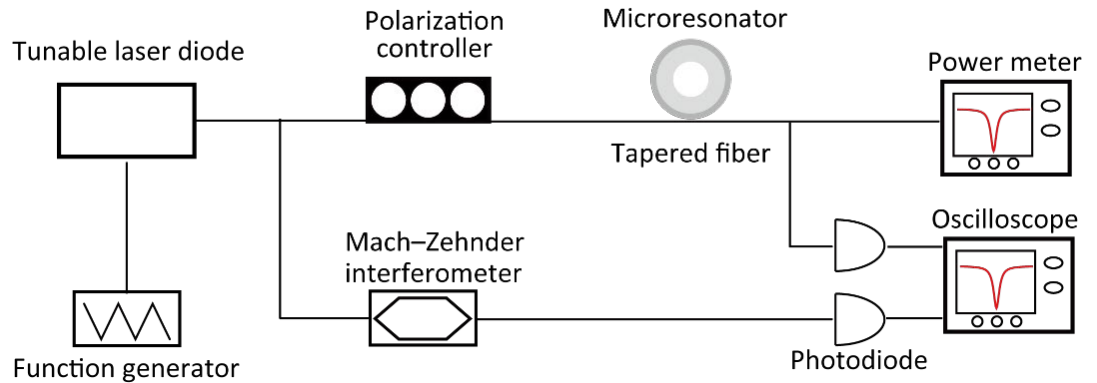
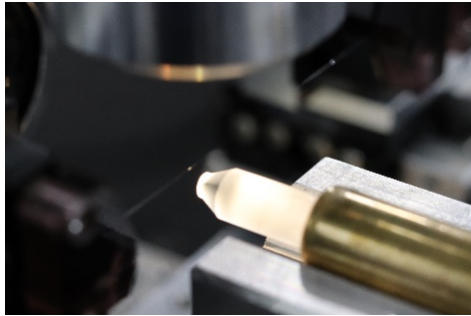
- High-Q of $> 10^8$ was obtained in MgF_2 spherical WGM resonator
- Effect of crystal anisotropy is investigated and we cut at an optimized end-face direction
- MgF_2 is more suitable for Kerr comb generation as regards thermal stability



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Experimental setup for Q-factor and dispersion measurement



Group-velocity dispersion

$D_2 > 0$: anomalous
 $D_2 < 0$: normal

Resonance frequency:
$$\omega_m = \frac{2\pi mc}{Ln(\omega)}$$

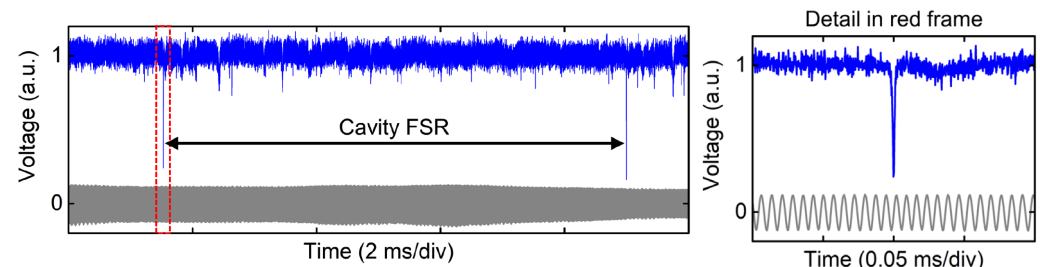
Resonance frequencies are Taylor-expanded:

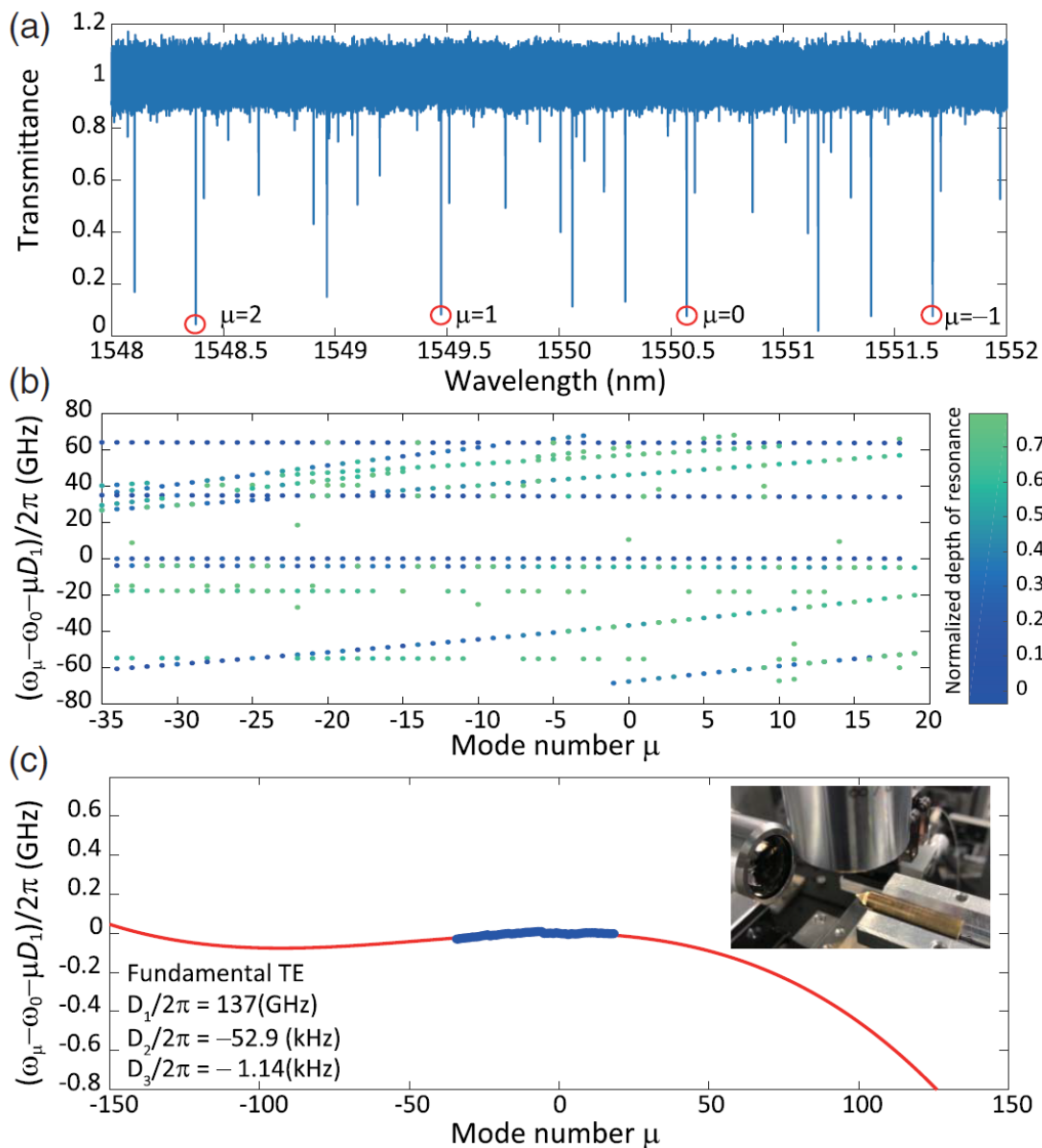
$$\omega_\mu = \omega_0 + D_1\mu + \frac{1}{2}D_2\mu^2 + \frac{1}{6}D_3\mu^3 + \dots$$

m : mode number

μ : mode number offset (from pump $\mu = 0$)

Mach-Zehnder interferometer calibrates frequency axis

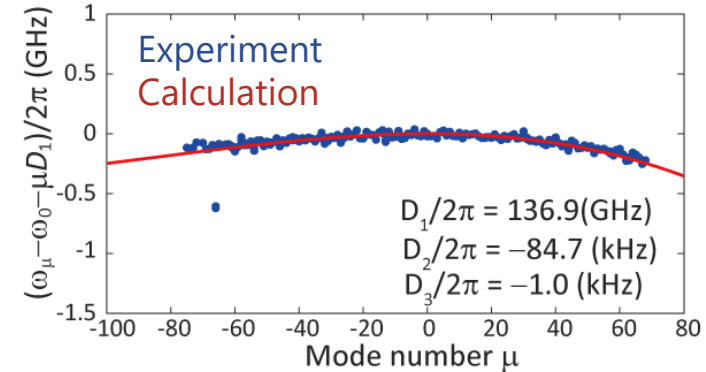
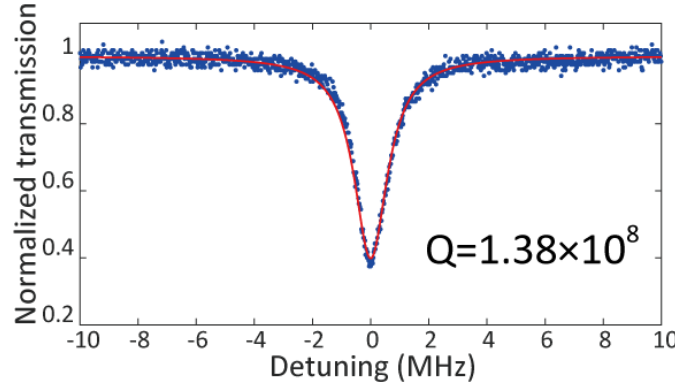
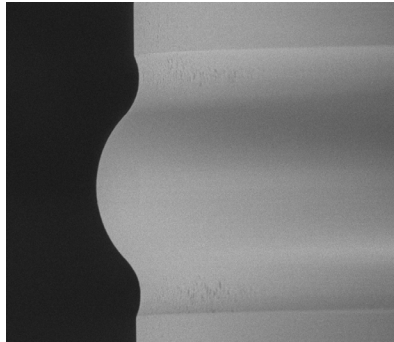




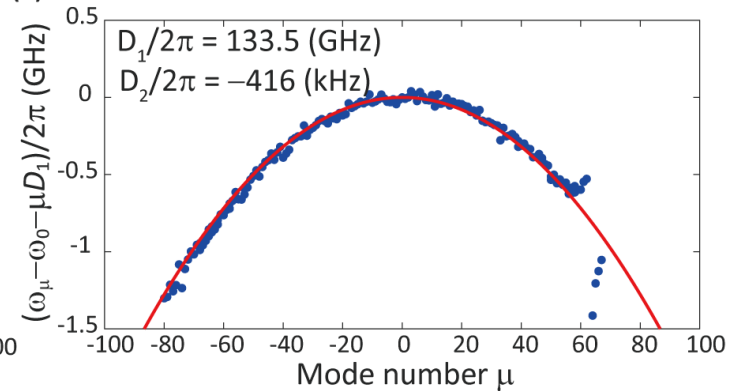
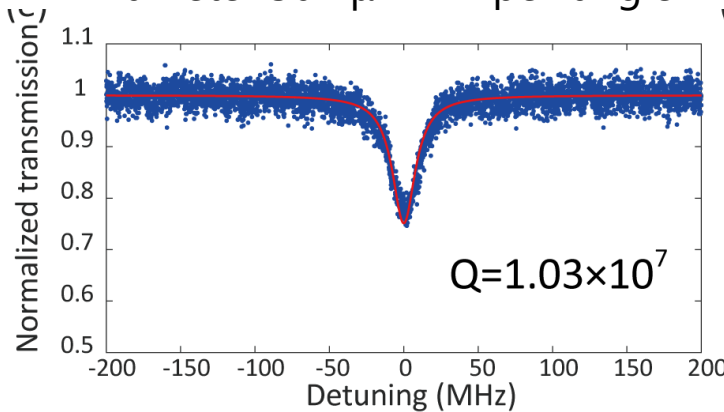
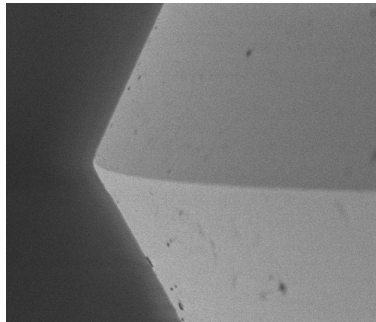


Crystalline microresonator fabricated "*without polishing*"

Spherical MgF_2 WGM Diameter 508 μm Curvature 36 μm



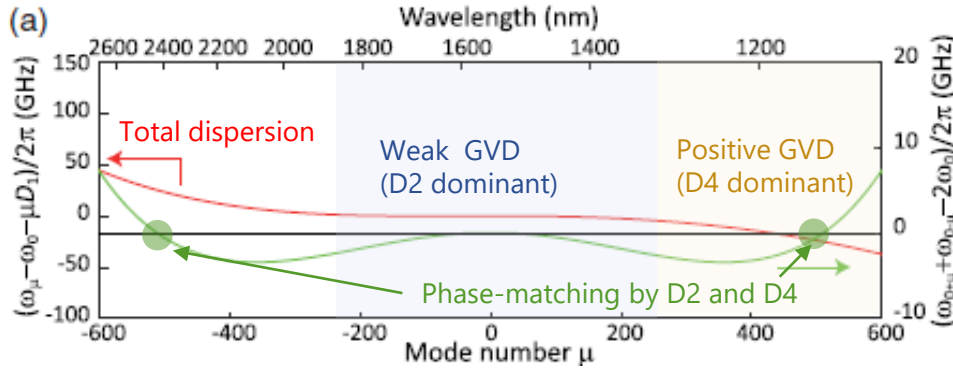
Triangular CaF_2 WGM Diameter 502 μm Apex angle 120°



- High-Q of $> 10^8$ was obtained in MgF_2 spherical WGM resonator
- Designed dispersion is obtained



- Principle: Negative GVD ($D_2 < 0$) is compensated by positive D_4 far from the pump mode



Phase-matching condition (PMC) for initial sidebands μ

$$\Delta\omega = \omega_\mu - \omega_0 - (\omega_0 - \omega_{-\mu}) = D_2\mu^2 + \frac{D_4}{12}\mu^4 \rightarrow 0$$

$$\mu^2 = -\frac{12D_2}{D_4} \quad (D_2 \cdot D_4 < 0)$$

Negative D_2 and Positive D_4 satisfy PMC far from the pump
Strong negative D_2 enables large frequency shift

- Numerical simulation (LLE)

LLE (Lugiato-Lefever equation) w/ all order dispersion

$$\frac{\partial A(\phi, t)}{\partial t} = -\left(\frac{\kappa_{tot}}{2} + i\delta_0\right)A + i\sum_{k=2} \frac{D_k}{k!} \left(\frac{\partial}{i\partial\phi}\right)^k A + ig|A|^2A + \sqrt{\kappa_{ext}}A_{in}$$

κ_{tot} : loaded decay rate ($Q_{tot} = \omega_0/\kappa_{tot}$)

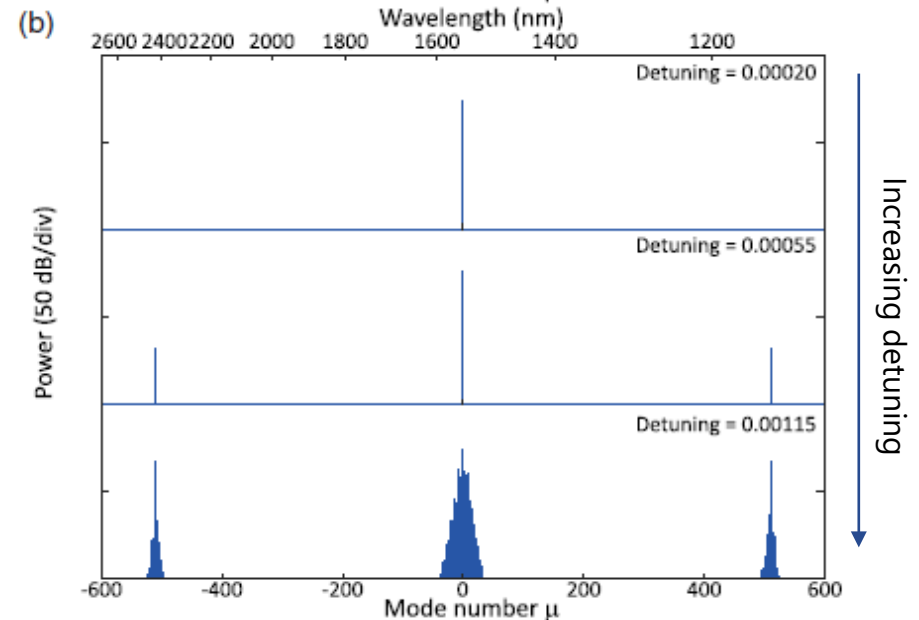
κ_{ext} : coupling rate ($Q_{ext} = \omega_0/\kappa_{ext}$)

δ_0 : pump detuning

D_k : k -order dispersion ($k \geq 2$)

g : nonlinear coefficient

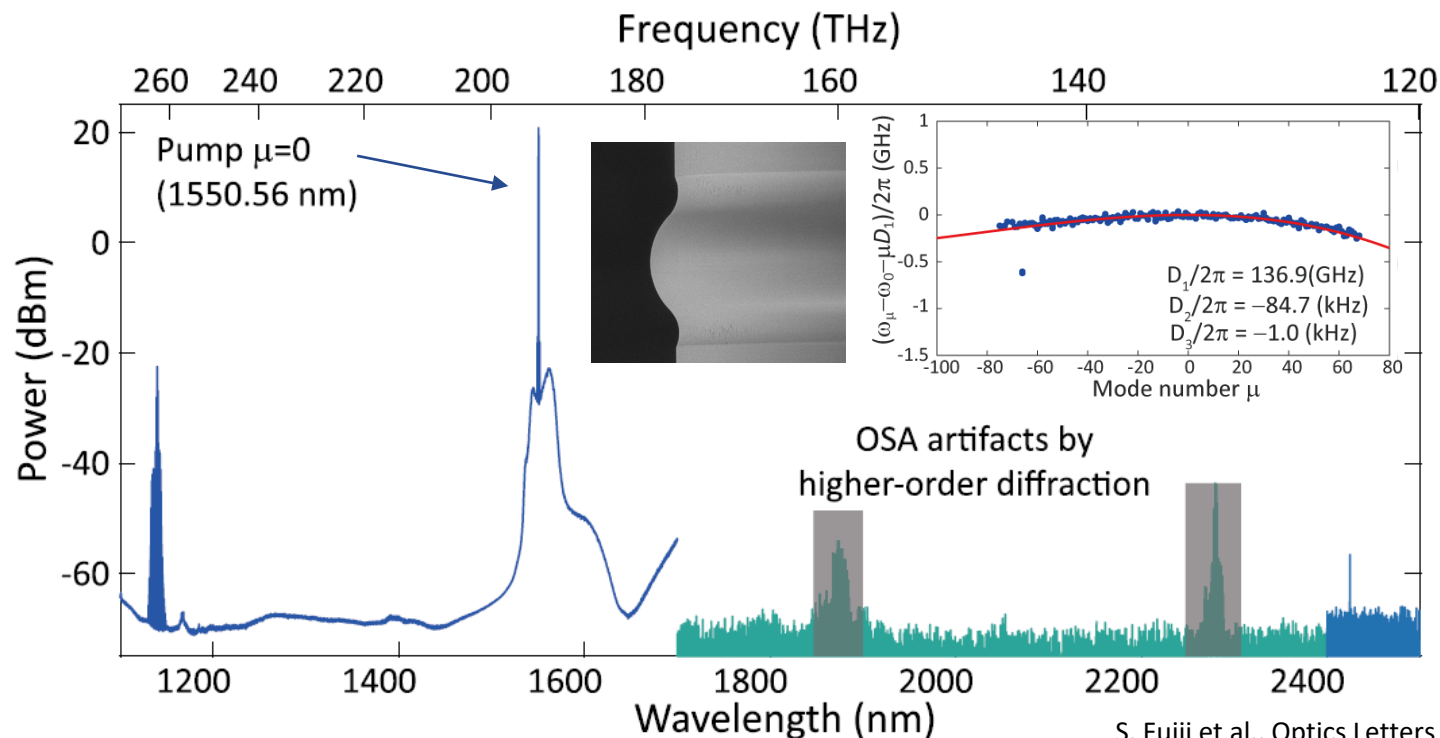
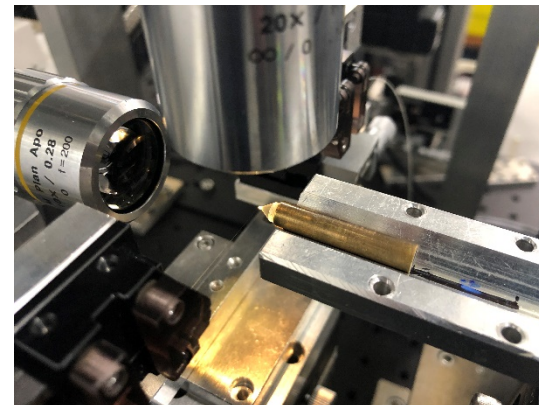
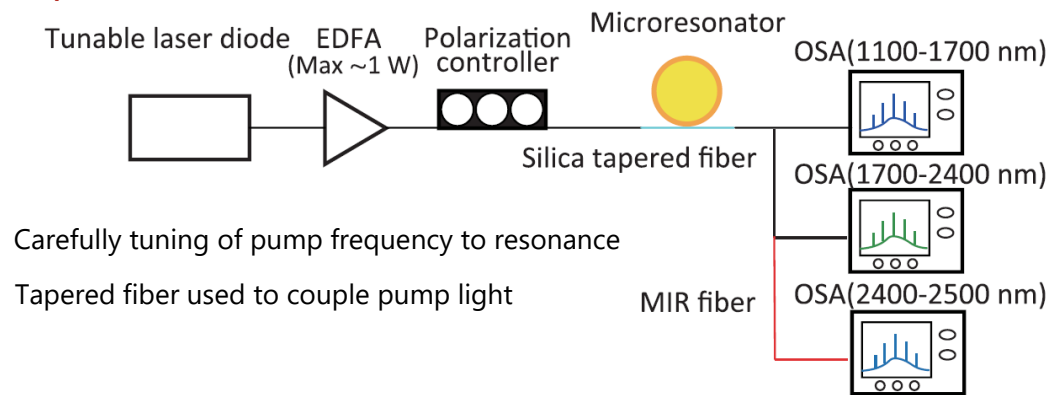
A_{in} : input field (pump)



- FWM sidebands spanning one-octave via higher-order dispersion (4th order dispersion)

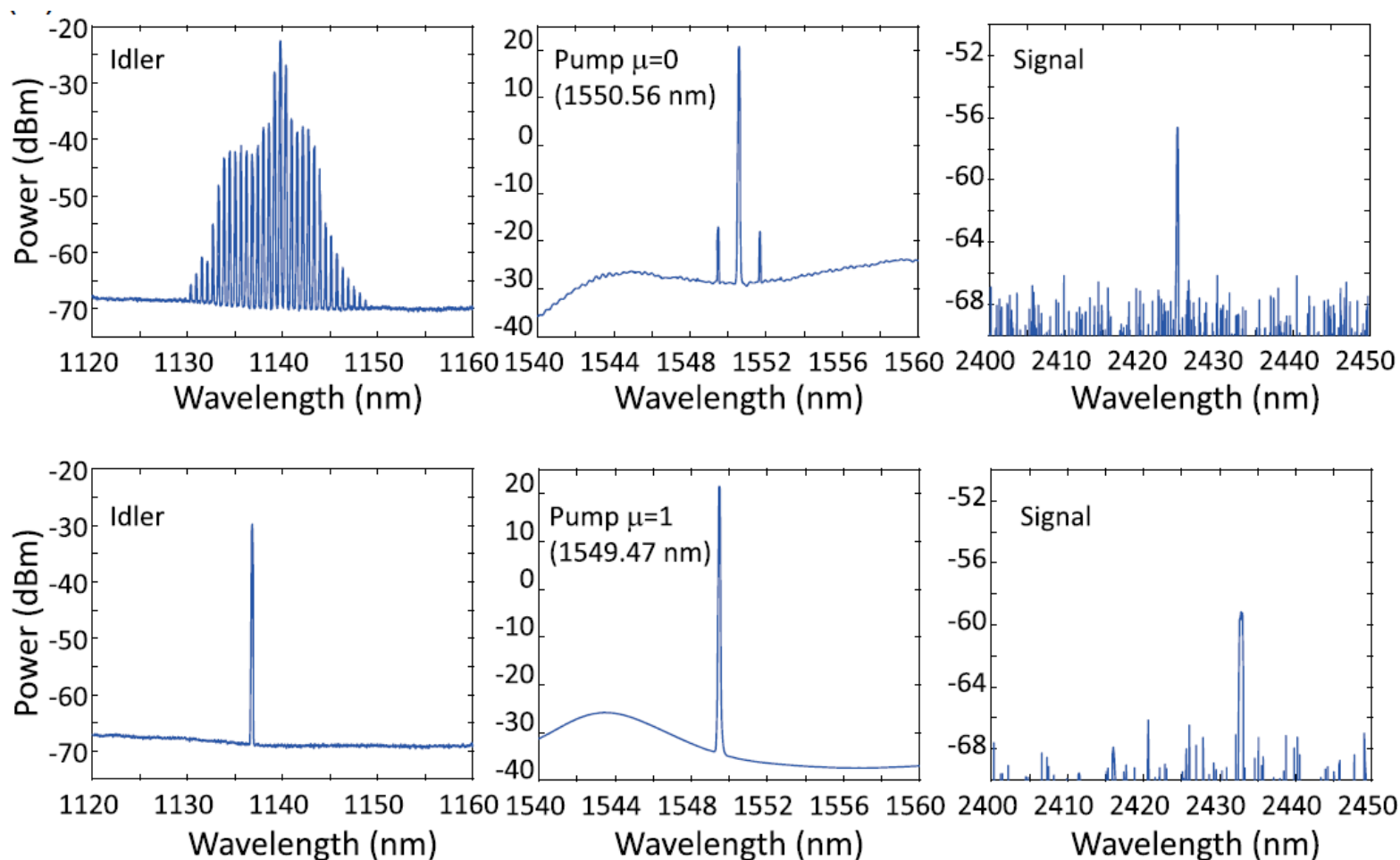


- Experiment



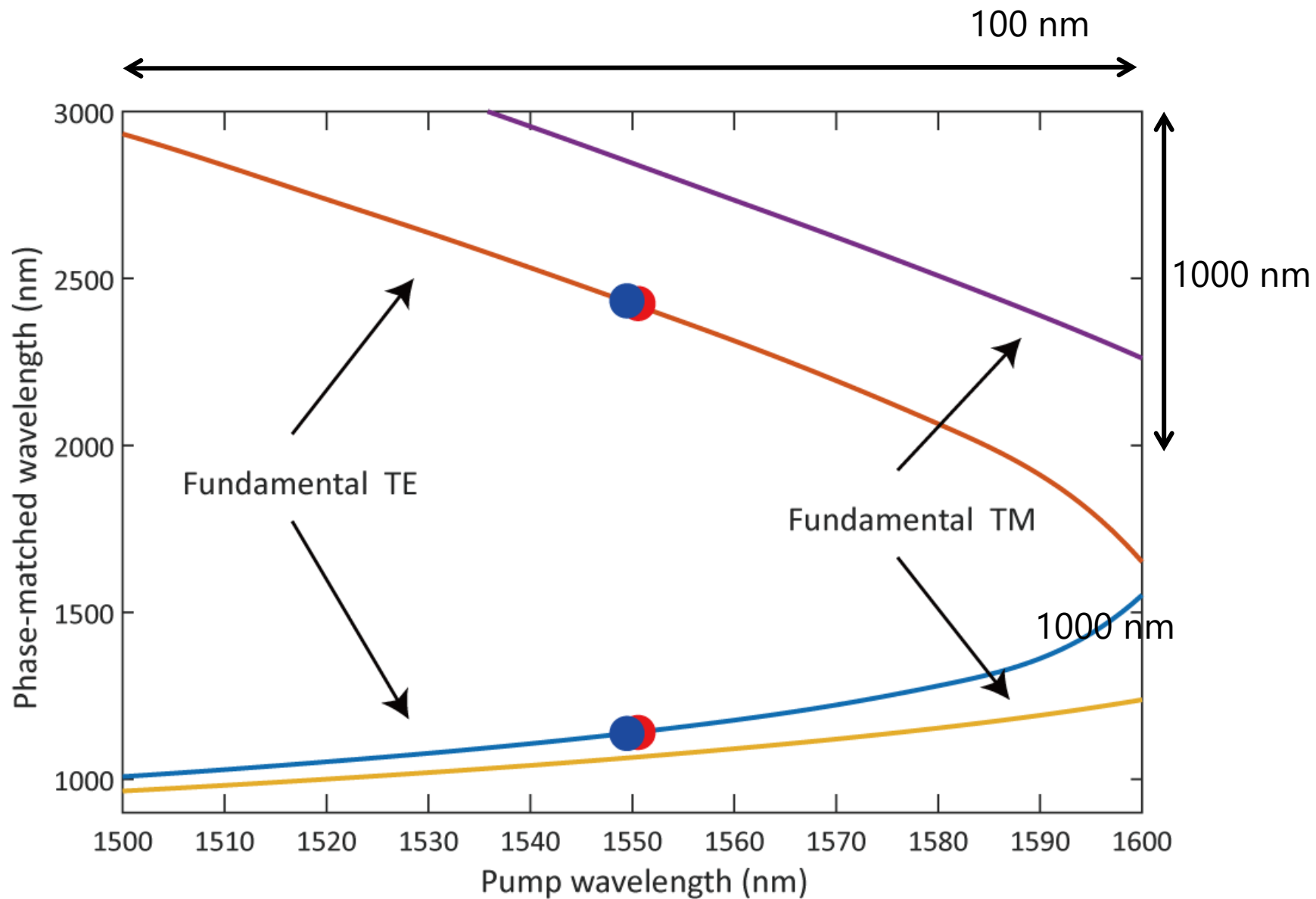


- Experiment



S. Fujii et al., Optics Letters 44, 3146 (2019).

- Shorter wavelength pump allows us to obtain larger frequency shift by the balance between D2 and D4 (Tunability of oscillation wavelegnth)





- Proposed ideal WGM structure for 100-GHz FSR microcomb in MgF_2 crystalline microresonators (rectangular shapes achieve anomalous dispersion in 1550 nm)
- Identified critical depth and for each end-face orientation to achieve ultra-precision machining of crystalline microresonators
- Observed highest Q exceeding 10^8 and microcomb without polishing process
- Demonstrated octave-wide FWM in dispersion-engineered microresonators

Thank you

Publication

S. Fujii et al., "Octave-wide phase-matched four-wave mixing in dispersion engineered crystalline microresonators", Optics Letters **44**, 3146 (2019).

Acknowledgment

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We thank Dr. Y. Mizumoto, H. Kangawa for their contribution of this work